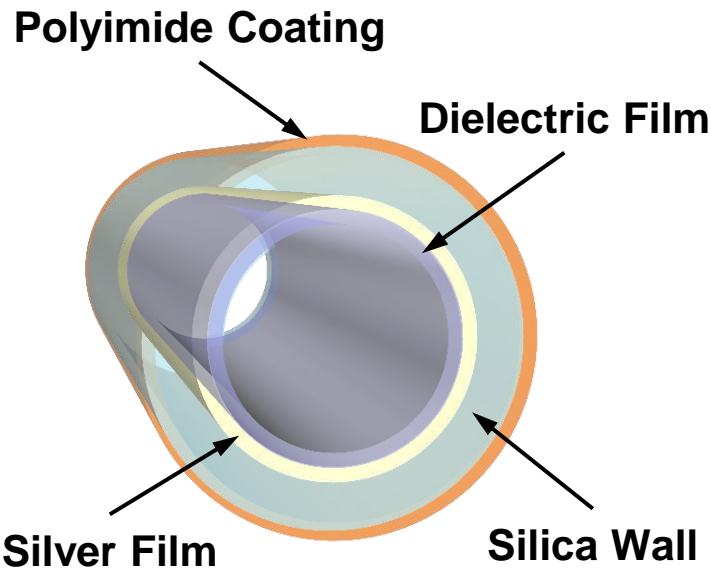


Silver / Polystyrene Coated Hollow Glass Waveguides for the Transmission of Visible and Infrared Radiation

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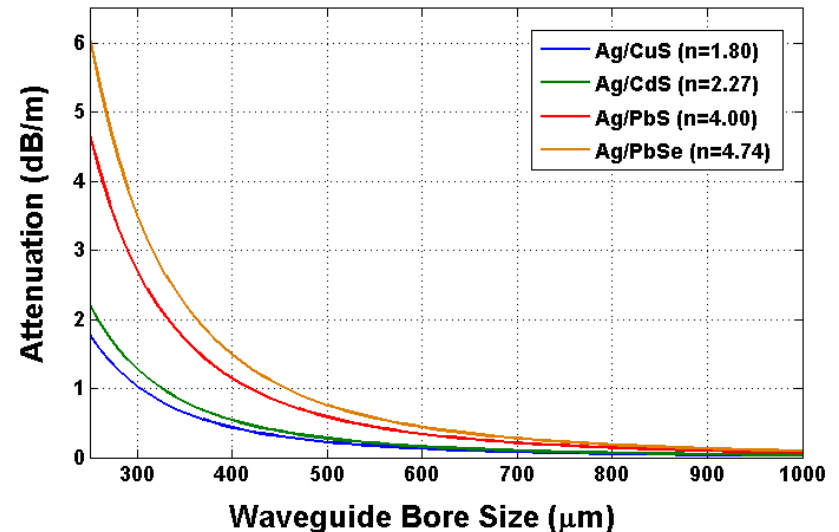
- Used in the low loss broadband transmission from $\lambda = 1 - 16 \mu\text{m}$
- Light propagation due to enhanced inner wall surface reflection



• Structure of HGWs

- SiO_2 capillary tubing substrate
- Ag film ~200 nm thick
- Dielectric(s) such as AgI, CdS, PbS
- Multilayer structures of interest

- Theoretical loss dependence *
 - $\propto 1/a^3$ (a is bore radius)
 - $\propto 1/R$ (R is bending radius)



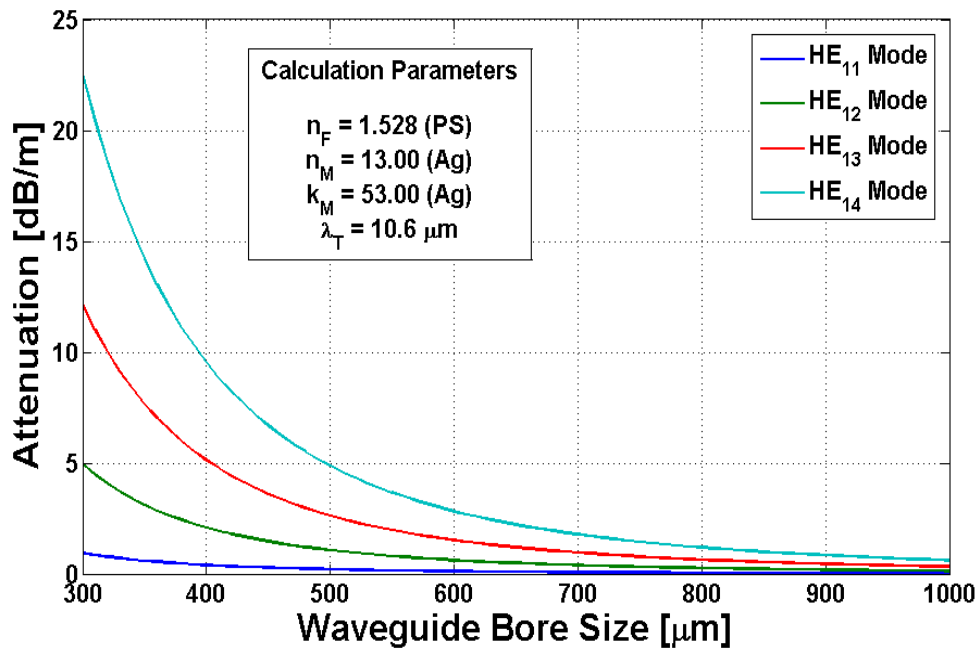
* Harrington, J. A., Infrared Fiber Optics and Their Applications

- Practical losses in HGWs:
 - Propagating modes
 - Dielectric thin film materials
 - Thickness of deposited films
 - Quality and roughness of films
 - Number of films deposited
 - \uparrow Throughput \propto \downarrow mode quality

Wave Optics Attenuation Equation

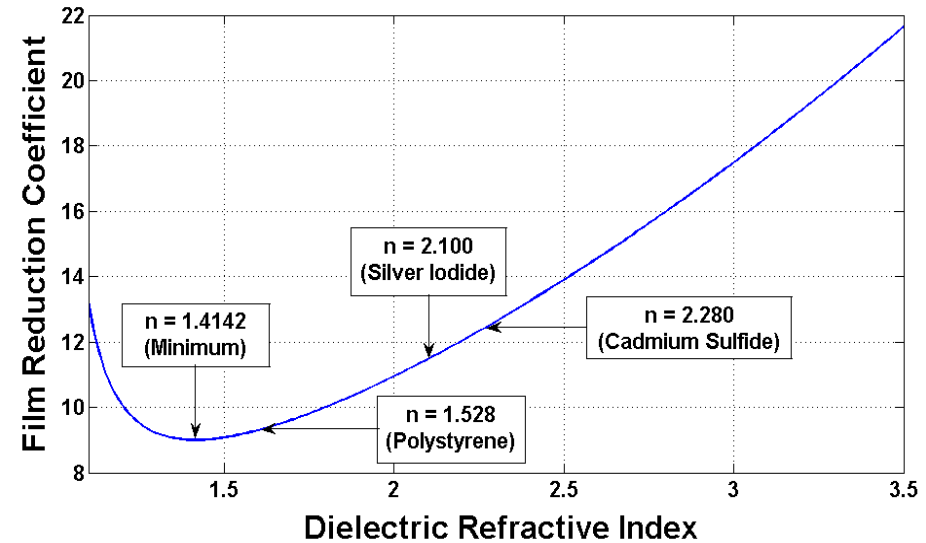
$$\alpha = \left(\frac{u_{nm}}{2\pi} \right)^2 \frac{\lambda^2}{a^3} \left(\frac{n_m}{n_m + k_m} \right) F_{film}$$

u_{nm} = mode parameter
 λ = wavelength
 a = HGW inner radius size
 n_m = metal refractive index
 k_m = metal absorption coefficient
 F_{film} = film loss reduction term



- F_{film} term dependence on:
 - Thin film structure
 - Propagating mode(s)
- TE₀₁ mode is lowest loss mode in metal / dielectric coated HWs
- HE₁₁ mode is lowest loss mode in metal / dielectric coated HWs

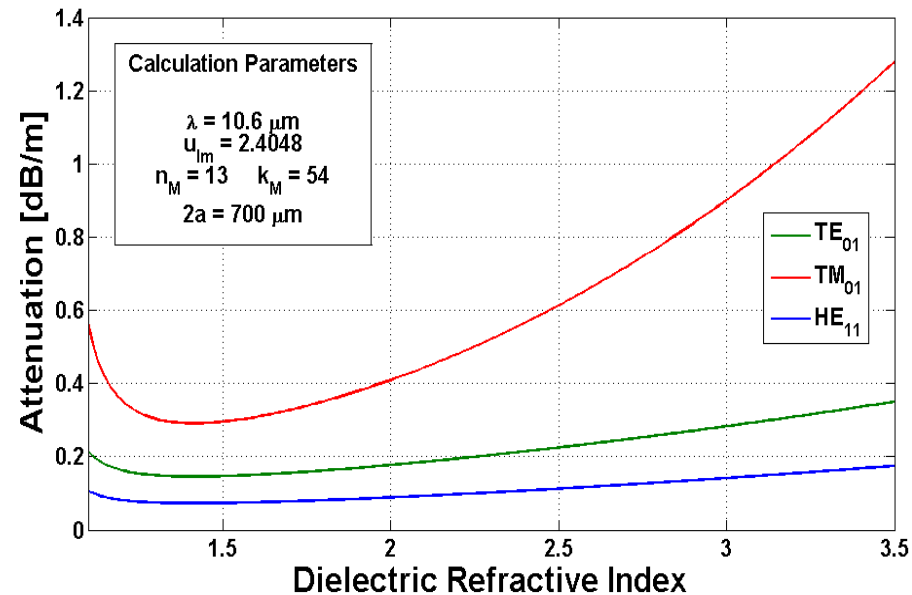
- Effect of dielectric layer on HGW
 - Constructive thin film interference
 - Reflection enhancement
 - Change in lowest loss mode
 - $TE_{01} \rightarrow HE_{11}$
 - Lower bending losses



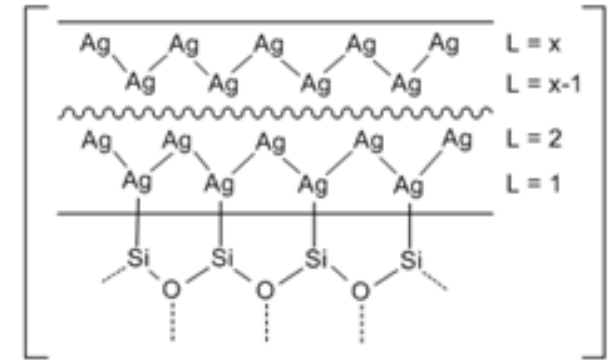
Single Dielectric Film Loss Reduction

$$F_{film} = \begin{cases} \left(1 + \frac{n_d^2}{\sqrt{n_d^2 - 1}}\right) & TE_{0m} \\ \frac{n_d^2}{\sqrt{n_d^2 - 1}} \left(1 + \frac{n_d^2}{\sqrt{n_d^2 - 1}}\right) & TM_{0m} \\ \frac{1}{2} \left(1 + \frac{n_d^2}{\sqrt{n_d^2 - 1}}\right) & HE_{1m} \end{cases}$$

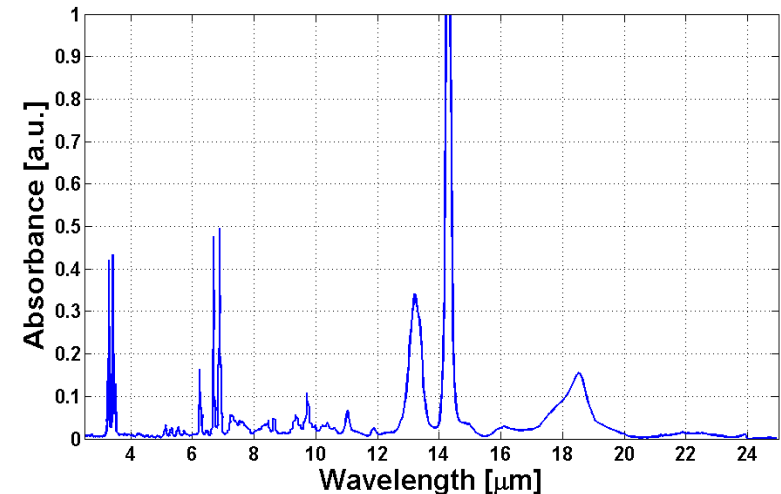
n_d = dielectric refractive index



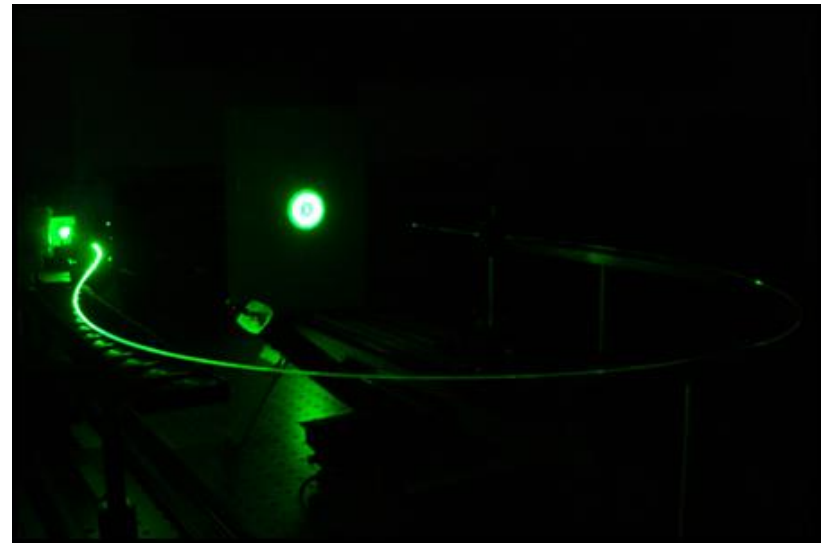
- Advantages of Ag coated HGWs:
 - High laser damage threshold (CW & pulsed laser propagation)
 - No end reflection losses
 - Capable of broadband transmission (air core)
 - Reliability & durability in applications
 - Relatively low manufacturing costs



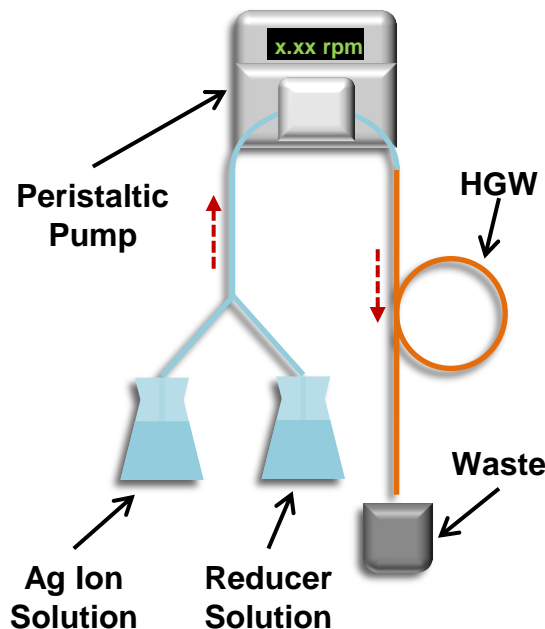
- Advantages of Ag / PS coated HGWs:
 - Close to optimal refractive index of $n = 1.414$
 - Very low-loss HGW dielectric film material
 - PS transparency from 500 nm to $> 100 \mu\text{m}$
 - Dielectric for VIS, IR, and THz λ
 - Chemically inert / high durability
 - Protective / optically functional coating
 - Inexpensive material / Non-hazardous
 - HE_{11} mode propagation



- Research objectives:
 - Optimize Ag deposition procedure to $\downarrow \alpha$
 - Fabrication of low-loss HGWs at visible λ of longer lengths
 - Deposition of PS thin films in Ag coated HGWs for:
 - Low-loss transmission at visible λ (500 – 700 nm)
 - Low-loss transmission at NIR λ (800 – 1500 nm)
 - Low-loss transmission at THz λ ($> 100 \mu\text{m}$)
- Experimental Approach
 - Dimensionality constant at ID = 1000 μm
 - Optimize Ag deposition procedure by:
 - Varying fabrication parameters
 - Reducing manufacturing defects
 - Deposition of PS dielectric thin films
 - Control of deposition parameters
 - Increase reliability & consistency
 - Characterization to include:
 - FTIR spectroscopy
 - Optical attenuation measurements

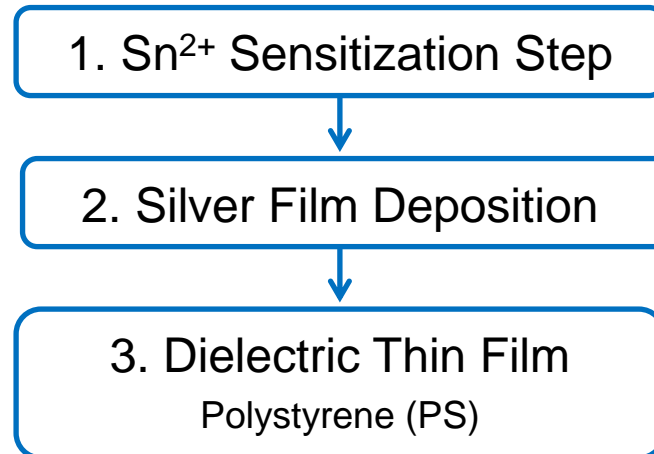
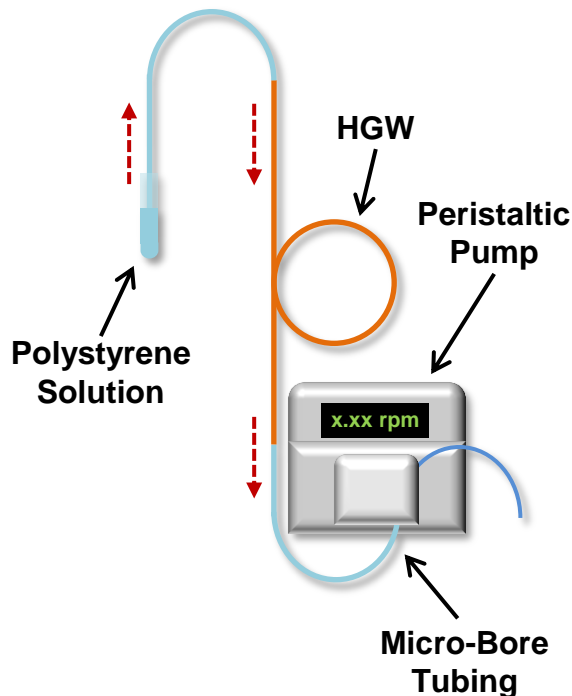


- Films deposited via dynamic liquid phase deposition process (DLPD)
- Factors with major influence on Ag film quality
 - Solution concentrations (particularly Ag ion & reducer solutions)
 - Temperature of solutions (influences film growth rate)
 - Fluid flow rate (optimal flow velocity at ≈ 75 cm/s)
 - Atmospheric lighting (UV exposure results in low quality films)



- Optimization of Ag deposition procedure
 - Improve film quality \rightarrow lower α at shorter λ
 - Applications at visible & NIR wavelengths
 - Fabrication of longer HGW samples (> 5 m)
- Key experimental parameters
 - Solution concentrations
 - Sensitizing procedure time
 - **Silver deposition time**
 - Fluid flow rate

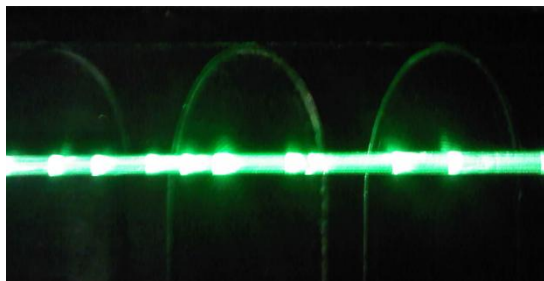
- Films deposited via modified DLPD procedure
- The DLPD process for deposition of PS films:
 - PS deposition technique based on viscous drag rather than chemical reactions
 - Considerably harder to deposit uniform films along long HGW lengths
 - Vacuum pull technique used to pull polystyrene in organic solvent solution



- PS film quality and thickness control
 - Variation of pump pulling rate
 - **Variation of PS solution concentration**
 - Variation of organic solvent used

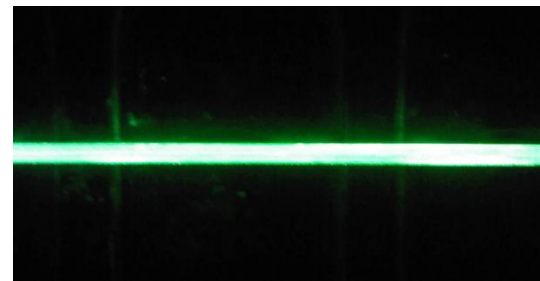
- Effect of sensitization procedure:
 - Reduction of Ag deposition time from 20 – 30 min → 2 – 3 min (~ 10×)
 - Optimal sensitization parameters:
 - $[\text{SnCl}_2] = 1.55 \text{ mM}$ @ pH ≈ 4.3
 - Sensitization time of 5 min followed by 7.5 min drying time
- Effect of deposition fluid flow rate:
 - High correlation between fluid flow rate (VFR) & film quality

Low Fluid Flow Rates



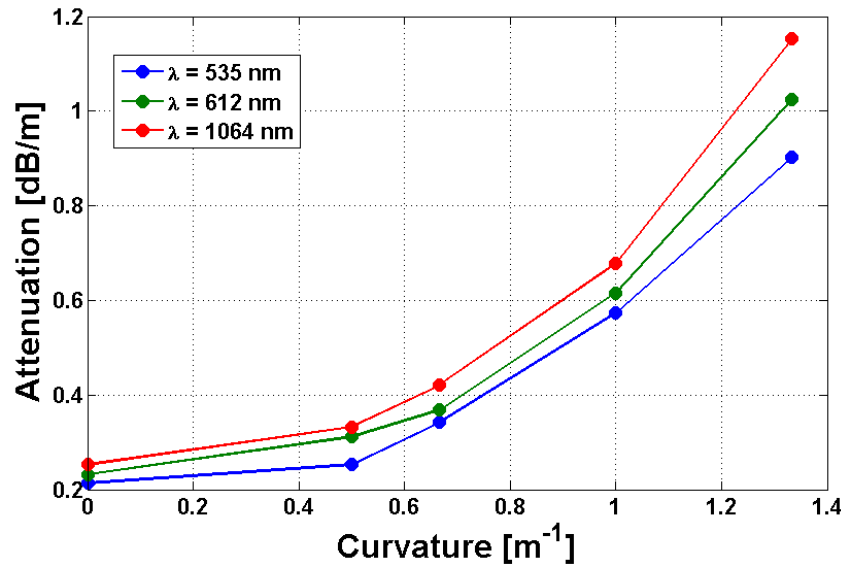
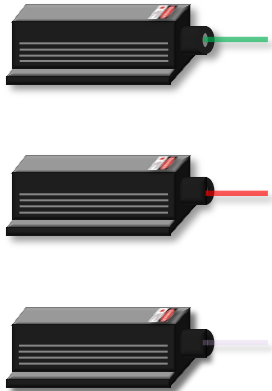
- Occasional 'striping' defects
- Non-uniform film quality
- Localized defects due to flow
- Length varying coating rate
- Generally for VFR < 20 mL/min

High Fluid Flow Rates



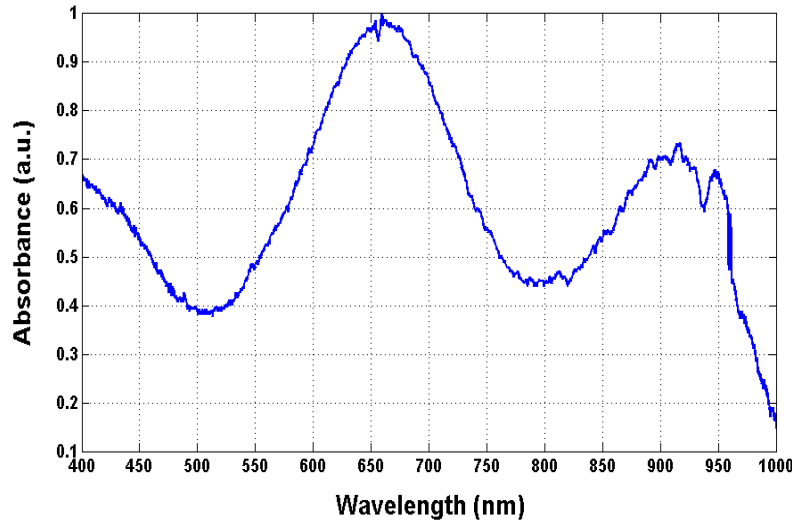
- Few or none 'striping' defects
- Uniform film quality
- Reduction of defect occurrence
- Uniform coating rate
- Generally for VFR > 40 mL/min

- Effect of Ag deposition time:
 - Minimize Ag deposition time while attaining adequate Ag film thickness
 - Optimal Ag deposition parameters:
 - $[Ag^{2+}] = 7.18 \text{ mM @ pH} \approx 9.5$ $[C_6H_{12}] = 1.55 \text{ mM}$
 - Optimal Ag deposition time of 180 – 195 sec at VFR $\approx 45 \text{ mL/min}$
- Attenuation measurements at VIS & NIR wavelengths
 - Loss measurements taken at $\lambda = 535 \text{ nm}$, 612 nm , and 1064 nm



- Able to fabricate samples at $L > 5.0 \text{ m}$ with measured $\alpha \sim 0.25 \text{ dB/m @ } \lambda = 535 \text{ nm}$

- Polystyrene is transparent at VIS & NIR wavelengths

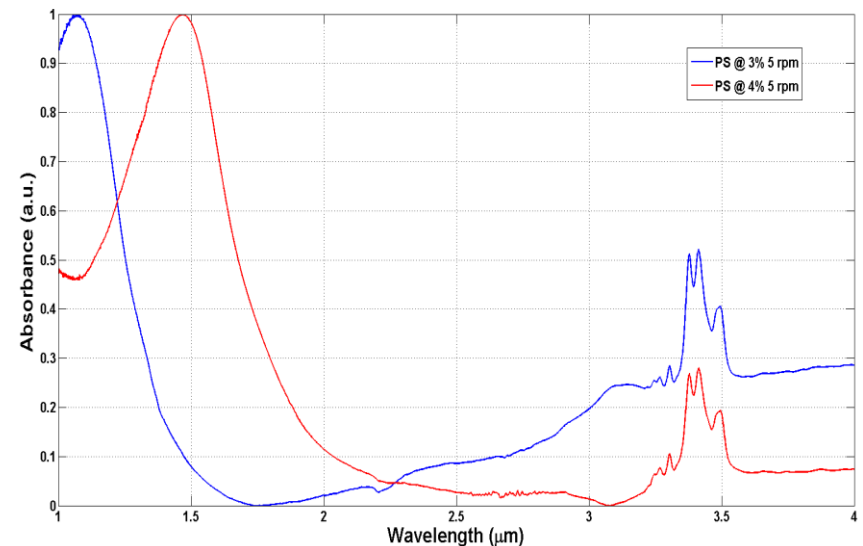


- VIS spectral analysis

- Uniform PS films at 0.5 & 1 wt % PS
- PS adequate dielectric for $\lambda = > 500 \text{ nm}$
- Film thicknesses: 0.1 – 0.2 μm
- Attenuation measurements to follow
- Thinner PS films necessary

- NIR spectral analysis

- Uniform PS films at 3 & 4 wt % PS
- PS adequate dielectric for $\lambda = 1 - 3 \mu\text{m}$
- Film thicknesses: 0.2 – 0.6 μm
- Attenuation measurements to follow
- Possibility for simultaneous λT



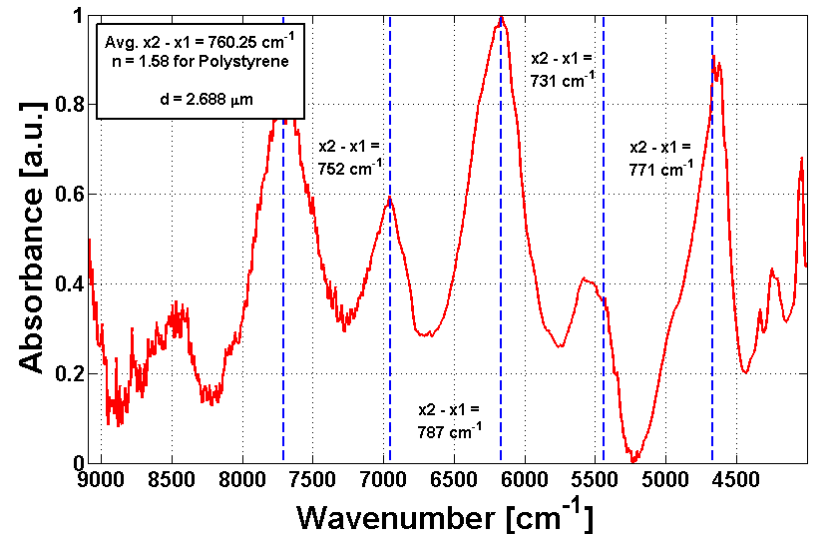
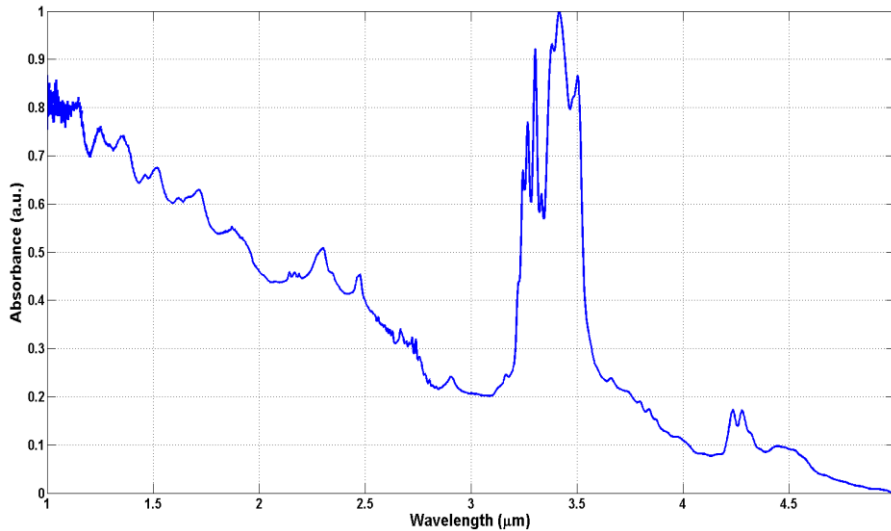
- Polystyrene thin films can be extended for THz λ transmission
- PS thin films of adequate thicknesses for THz transmission deposited
 - Film thicknesses from $> 1 \mu\text{m}$

$$d = \frac{(k_m - k_{m-1})^{-1}}{4 \cdot \sqrt{n_F^2 - 1}}$$

m = interference peak order

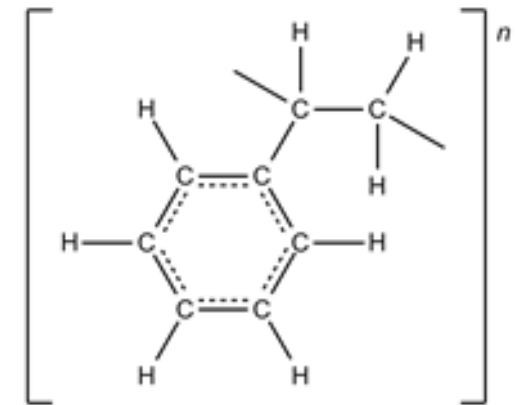
k = interference peak wavenumber

n_F = dielectric refractive index



- PS deposition procedure for THz
 - High [PS] solutions (22 – 28 weight %)
 - Thicknesses found through extrapolation
 - Losses $\sim 1.5 \text{ dB/m}$ at 2.9 THz

- Substantial improvement of Ag coated HGWs
 - Improvement of Ag film quality through fabrication optimization
 - Considerable decrease in loss at VIS & NIR wavelengths
 - Fabrication of low-loss HGWs > 5 m in length
 - Necessary reproducibility achieved
 - High power (> 1 MW) laser delivery attained
 - Pulsed laser at $\lambda = 535$ nm
- PS coatings in HGWs:
 - Successful deposition of PS thin films via DLPD
 - Further film quality control necessary
 - Continue development of coating techniques
 - Promising measured losses at THz frequencies
- Future research:
 - Continue improvement of PS thin film deposition procedure
 - Acquire consistent solution concentration / film thickness dependency
 - Comparison of Ag/PS HGWs vs. Ag HGWs at VIS & NIR λ
 - Fabrication of Ag/PS HGWs capable of low-loss THz λ delivery



Thank you for your attention!

